# Trend Analyses of Critical Values Obtained for Overall Nodes Extra Energy Savings Achievable in Ubicomp MANET Against Direct Node-to-Node Location-Aware Transmission.

M. Kaleem GALAMALI, Assoc. Prof Nawaz MOHAMUDALLY

Abstract - Quite extensive research is well ongoing concerning enhancements of location-tracking, MANET transmission and location-aware transmission for ubicomp [1-48]. Presently, more significant developments must be awaited before these three undergo successful merging and bring desirable improvements in ubicomp. One essential factor for success of this merging is correct protocol designs. At present era of technology, research in protocol designs are claimed as inapt for implementations due to present heuristic approaches [86]. Enhancements are also awaited in middleware services and applications [87]. Rework in ubicomp network architecture is also demanded [88]. A distant milestone in this direction of study is to fulfil realism in design and evaluation of wireless routing protocols [89]. Such direction of research will also output more usable components for predictability in ubicomp. Realism is tiresome to fulfil since it will cover each aspect related to ubicomp. One aspect was studied in a past research [17] to assess trend of extra energy savings achievable by overall nodes in MANETs (OLNTNES) against direct Node-to-Node transmission under different sets of node densities in a ubicomp environment. This study was reinforced by the corresponding study of trends for each OLNTNES parameter of equations [33].

To upgrade realism of these trends, in this paper, the next level of probing that is required is stated as: "What are the observable critical values in OLNTNES trends and the trends of these critical values?"

Such knowledge will gradually lead to the design of more realistic ubicomp scenarios over which experimental ubicomp features and communication protocols are tested validly. This paper follows-up from previous ones [1-48].

Key terms: Ubicomp- Ubiquitous Computing, MAUC- Mobile and Ubiquitous Computing, ES- Energy Savings, OLNTNES-Overall Less Node-to-Node ES, CBR- Constant Bit Rate, MANET- Mobile Adhoc Network, CV- Critical Value.

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# **1. Introduction**

A significantly wide range of factors affect energy consumption in MAUC [2]; type of transmission and node density remain predominant ones. In a past research [17], a simulation endeavour was carried out to derive the particular trend/model which depicts the overall nodes extra energy savings achievable against direct node-to-node transmission in MANET (OLNTNES) compared to theoretical/empirical models derived in simulations. The model put forward for metric OLNTNES was the normal distribution model:  $F(x) = b*(1/(a*sqrt(2*pi)))*exp(-(x-c)^2/2*a*a)$ 

Obviously, the study which followed [33] was mathematical modelling of the trends of the three parameters of equation obtained, so that the results may serve towards better understanding of the evolution and predictability of ubicomp environments. As progress is made in this direction, designers may produce a platform of newly developed components, including communication protocols and middleware functions, can be exercised convincingly.

The next stage of investigation required for metric OLNTNES is identifying observable critical values obtained during experimentations and formulating the corresponding mathematical trend of variations over varying node densities for each critical value. Nine such critical values have been observed.

The key contribution of this paper is the derivation of the trend of variation for each of the nine critical values observed for metric OLNTNES introduced in prior papers [17, 33], covering node numbers 7 until 56. Such data, if properly produced, will assist designers to better understand the evolution and predictability of ubicomp behaviour and derive more acceptable simulation scenarios over which new communication protocols being implemented could be reliably tested. The rest of this paper is organised as follows: section 2-OLNTNES Critical Values, section 3- Critical Values Trend Analyses- Metric OLNTNES, section 4-Conclusion and References.

# 2. OLNTNES Critical Values.

# 2.0 Critical Values Identified.

Nine critical values have been identified as follows: Column headings are:  $C1 \rightarrow OLNTNES \ CV, \ C2 \rightarrow$ Meaning of OLNTNES CV,  $C3 \rightarrow$  Corresponding figure number for the OLNTNES CV.



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C1	C2	C3
1	Smallest OLNTNES value obtained.	1
2	Highest value of OLNTNES obtained.	2
3	Experimental Modal value of OLNTNES.	3
4	%CBR with OLNTNES < modal value.	4
5	%CBR with OLNTNES > modal value.	5
6	%CBR with negative OLNTNES values.	6
7	%CBR with OLNTNES value 0.	7
8	%CBR with positive OLNTNES values.	8
9	95% CBR have OLNTNES value as from.	9
	Table 1: OLNTNES Critical Values	

# 2.1 Experimental Critical Values Obtained.

The values obtained in experiments are summarised below. Values have been rounded to a maximum of 9 decimal places Column heading NN  $\rightarrow$  Node Number

7         -1397         48         2         77.539682540         18.6507930           8         -1397         48         2         77.570837313         18.6564783           9         -1188         52         2         78.095238095         17.5396823           10         -1208         67         -5         66.031746032         30.9523809           11         -1175         65         -5         67.460317460         29.8412693           12         -1204         63         -11         58.251192369         39.268680           13         -1225         62         -13         53.650793651         43.571428           14         -1293         62         -14         54.3650793651         43.571428           16         -2321         62         -5         74.190476190         23.0317460           17         -3555         66         -30         35.158730159         62.380523           18         -4365         66         -15         59.23809523         38.015873           19         -3911         66         -17         56.825396825         40.7936507           20         -4021         66         -9         73.253968254	
8         -1397         48         2         77.570837313         18.6564783           9         -1188         52         2         78.095238095         17.539682           10         -1208         67         -5         66.031746032         30.9523809           11         -1175         65         -5         67.460317460         29.841269           12         -1204         63         -11         58.251192369         39.268680           13         -1225         62         -13         53.650793651         43.571428           14         -1293         62         -14         54.365079365         42.666666           15         -1690         62         -20         45.761904762         51.8571428           16         -2321         62         -5         74.190476190         23.031746           17         -3555         66         -30         35.158730159         62.380952           18         -4365         66         -15         59.238095238         38.0158730           19         -3911         66         -17         56.825396825         40.793650           20         -4021         66         -9         73.253968254	551
9         -1188         52         2         78.095238095         17.539682           10         -1208         67         -5         66.031746032         30.9523800           11         -1175         65         -5         67.460317460         29.841269           12         -1204         63         -11         58.251192369         39.268680           13         -1225         62         -13         53.650793651         43.571428           14         -1293         62         -14         54.365079365         42.6666666           15         -1690         62         -20         45.761904762         51.8571428           16         -2321         62         -5         74.190476190         23.031746           17         -3555         66         -30         35.158730159         62.3809528           18         -4365         66         -15         59.238095238         38.015873           19         -3911         66         -17         56.825396825         40.793650           20         -4021         66         -9         73.253968254         24.2857142           21         -1790         70         -12         67.61904762	328
10 $-1208$ 67 $-5$ 66.03174603230.95238011 $-1175$ 65 $-5$ 67.46031746029.84126912 $-1204$ 63 $-11$ 58.25119236939.26868013 $-1225$ 62 $-13$ 53.65079365143.57142814 $-1293$ 62 $-14$ 54.36507936542.66666615 $-1690$ 62 $-20$ 45.76190476251.857142816 $-2321$ 62 $-5$ 74.19047619023.031746617 $-3555$ 66 $-30$ 35.15873015962.380952218 $-4365$ 66 $-15$ 59.23809523838.01587319 $-3911$ 66 $-17$ 56.82539682540.793650720 $-4021$ 66 $-9$ 73.25396825424.285714221 $-1790$ 70 $-12$ 67.69841269829.68253922 $-2887$ 70 $-12$ 69.12698412728.253968223 $-3824$ 70 $-17$ 60.31746031737.30158724 $-3153$ 70 $-15$ 65.2222222232.460317425 $-2283$ 70 $-13$ 69.76190476227.873015926 $-3238$ 72 $-13$ 68.888888928.730158727 $-3220$ 72 $-17$ 62.85714285734.682539728 $-3138$ 72 $-15$ 67.85714285734.682539730 $-3233$ 72 $-23$ 56.03174603241.50793631 $-1637$ <t< td=""><td>540</td></t<>	540
11       -1175       65       -5       67.460317460       29.8412699         12       -1204       63       -11       58.251192369       39.268680         13       -1225       62       -13       53.650793651       43.571428         14       -1293       62       -14       54.365079365       42.666666         15       -1690       62       -20       45.761904762       51.8571423         16       -2321       62       -5       74.190476190       23.0317460         17       -3555       66       -30       35.158730159       62.3809522         18       -4365       66       -15       59.238095238       38.0158730         19       -3911       66       -17       56.825396825       40.7936507         20       -4021       66       -9       73.253968254       24.2857142         21       -1790       70       -12       67.698412698       29.6825399         22       -2887       70       -13       69.761904762       27.8730159         23       -3824       70       -13       69.761904762       27.8730159         24       -3153       70       -15       67.57142	952
12       -1204       63       -11       58.251192369       39.268680.         13       -1225       62       -13       53.650793651       43.571428.         14       -1293       62       -14       54.3650793651       42.666666.         15       -1690       62       -20       45.761904762       51.8571428.         16       -2321       62       -5       74.190476190       23.031746.         17       -3555       66       -30       35.158730159       62.380952.         18       -4365       66       -15       59.238095238       38.015873.         19       -3911       66       -17       56.825396825       40.793650.         20       -4021       66       -9       73.253968254       24.285714.         21       -1790       70       -12       67.698412698       29.682539.         22       -2887       70       -13       69.761904762       27.8730157         24       -3153       70       -15       65.22222222       32.460317.         25       -2283       70       -13       69.761904762       27.8730158.         27       -320       72       -17       62.	341
13         -1225         62         -13         53.650793651         43.5714283           14         -1293         62         -14         54.365079365         42.666666           15         -1690         62         -20         45.761904762         51.8571423           16         -2321         62         -5         74.190476190         23.0317466           17         -3555         66         -30         35.158730159         62.3809522           18         -4365         66         -15         59.238095238         38.015873           19         -3911         66         -17         56.825396825         40.793650           20         -4021         66         -9         73.253968254         24.2857142           21         -1790         70         -12         69.126984127         28.2539682           23         -3824         70         -17         60.317460317         37.301587           24         -3153         70         -13         69.761904762         27.8730159           26         -3238         72         -13         68.88888889         28.730158           27         -3220         72         -17         64.841269841 <td>445</td>	445
14       -1293       62       -14       54.365079365       42.6666666         15       -1690       62       -20       45.761904762       51.8571423         16       -2321       62       -5       74.190476190       23.0317460         17       -3555       66       -30       35.158730159       62.3809523         18       -4365       66       -15       59.238095238       38.0158733         19       -3911       66       -17       56.825396825       40.793650         20       -4021       66       -9       73.253968254       24.2857142         21       -1790       70       -12       67.698412698       29.682539         22       -2887       70       -12       69.126984127       28.2539682         23       -3824       70       -17       60.317460317       37.301587         24       -3153       70       -15       65.22222222       32.460317         25       -2283       70       -13       69.761904762       27.8730158         27       -3220       72       -17       62.857142857       34.6825399         28       -3138       72       -17       64.841269	571
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17 $-3555$ 66 $-30$ $35.158730159$ $62.38095238$ 18 $-4365$ 66 $-15$ $59.238095238$ $38.0158730$ 19 $-3911$ 66 $-17$ $56.8253968254$ $40.7936507$ 20 $-4021$ 66 $-9$ $73.253968254$ $24.2857142$ 21 $-1790$ 70 $-12$ $67.698412698$ $29.68253968254$ 22 $-2887$ 70 $-12$ $69.126984127$ $28.253968254$ 23 $-3824$ 70 $-17$ $60.317460317$ $37.301587736475766667666676766666666666666666666$	032
18       -4365       66       -15       59.238095238       38.0158730         19       -3911       66       -17       56.825396825       40.7936507         20       -4021       66       -9       73.253968254       24.2857142         21       -1790       70       -12       67.698412698       29.682539         22       -2887       70       -12       69.126984127       28.2539682         23       -3824       70       -17       60.317460317       37.3015872         24       -3153       70       -15       65.22222222       32.4603174         25       -2283       70       -13       69.761904762       27.87301587         26       -3238       72       -13       68.88888889       28.7301587         27       -3220       72       -17       62.857142857       34.6825399         28       -3138       72       -15       67.857142857       29.9365079         30       -3233       72       -23       56.031746032       41.507936         31       -1637       72       -19       61.746031746       36.0634920         32       -1682       72       -26       50.000	381
19         -3911         66         -17         56.825396825         40.793650           20         -4021         66         -9         73.253968254         24.2857142           21         -1790         70         -12         67.698412698         29.682539           22         -2887         70         -12         69.126984127         28.253968           23         -3824         70         -17         60.317460317         37.301587           24         -3153         70         -15         65.22222222         32.4603174           25         -2283         70         -13         69.761904762         27.8730158           26         -3238         72         -13         68.88888889         28.730158           27         -3220         72         -17         62.857142857         34.682539           28         -3138         72         -15         67.857142857         29.936507           29         -3188         72         -17         64.841269841         32.936507           30         -3233         72         -23         56.031746032         41.507936           31         -1637         72         -19         61.746031746	016
20       -4021       66       -9       73.253968254       24.2857147         21       -1790       70       -12       67.698412698       29.6825396         22       -2887       70       -12       69.126984127       28.253968         23       -3824       70       -17       60.317460317       37.301587         24       -3153       70       -15       65.22222222       32.460317         25       -2283       70       -13       69.761904762       27.8730158         26       -3238       72       -13       68.88888889       28.730158         27       -3220       72       -17       62.857142857       34.6825396         28       -3138       72       -15       67.857142857       29.936507         29       -3188       72       -17       64.841269841       32.936507         30       -3233       72       -23       56.031746032       41.507936         31       -1637       72       -19       61.746031746       36.063492         32       -1682       72       -26       50.000000000       47.698412         33       -1694       72       -28       47.857142857 </td <td>794</td>	794
21       -1790       70       -12       67.698412698       29.6825394         22       -2887       70       -12       69.126984127       28.2539683         23       -3824       70       -17       60.317460317       37.3015873         24       -3153       70       -15       65.22222222       32.4603174         25       -2283       70       -13       69.761904762       27.8730153         26       -3238       72       -13       68.88888889       28.730153         26       -3238       72       -13       68.88888889       28.730153         27       -3220       72       -17       62.857142857       34.6825394         28       -3138       72       -15       67.857142857       29.9365074         29       -3188       72       -17       64.841269841       32.9365074         30       -3233       72       -23       56.031746032       41.5079363         31       -1637       72       -19       61.746031746       36.0634920         32       -1682       72       -26       50.00000000       47.6984120         33       -1694       72       -28       47.85714	286
22       -2887       70       -12       69.126984127       28.2539682         23       -3824       70       -17       60.317460317       37.3015873         24       -3153       70       -15       65.22222222       32.4603174         25       -2283       70       -13       69.761904762       27.87301587         26       -3238       72       -13       68.88888889       28.7301587         26       -3238       72       -17       62.857142857       34.6825394         28       -3138       72       -15       67.857142857       29.9365074         29       -3188       72       -17       64.841269841       32.9365074         30       -3233       72       -23       56.031746032       41.5079363         31       -1637       72       -19       61.746031746       36.0634920         32       -1682       72       -26       50.000000000       47.6984120         33       -1689       72       -25       52.777777778       44.9206344         34       -1694       72       -28       47.857142857       49.603174         35       -1711       72       -20       62.4	583
23       -3824       70       -17       60.317460317       37.301587.         24       -3153       70       -15       65.22222222       32.460317.         25       -2283       70       -13       69.761904762       27.8730158         26       -3238       72       -13       68.88888889       28.730158         27       -3220       72       -17       62.857142857       34.6825399         28       -3138       72       -15       67.857142857       29.9365079         29       -3188       72       -17       64.841269841       32.9365079         30       -3233       72       -23       56.031746032       41.507936         31       -1637       72       -19       61.746031746       36.0634920         32       -1682       72       -26       50.000000000       47.6984120         33       -1689       72       -25       52.777777778       44.9206349         34       -1694       72       -28       47.857142857       49.603174         35       -1711       72       -20       62.444444444       51.158730         36       -1781       72       -28       50.31746	254
24       -3153       70       -15       65.222222222       32.4603174         25       -2283       70       -13       69.761904762       27.8730153         26       -3238       72       -13       68.888888889       28.730153         27       -3220       72       -17       62.857142857       34.6825399         28       -3138       72       -15       67.857142857       29.9365079         29       -3188       72       -17       64.841269841       32.9365079         30       -3233       72       -23       56.031746032       41.507936         31       -1637       72       -19       61.746031746       36.0634929         32       -1682       72       -26       50.000000000       47.6984129         33       -1689       72       -25       52.77777778       44.9206349         34       -1694       72       -28       47.857142857       49.6031746         35       -1711       72       -20       62.444444444       51.158730         36       -1781       72       -28       50.317460317       47.61904762         38       -1736       65       -14       73.01	302
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26 $-3238$ $72$ $-13$ $68.88888889$ $28.730158'$ $27$ $-3220$ $72$ $-17$ $62.857142857$ $34.6825396$ $28$ $-3138$ $72$ $-15$ $67.857142857$ $29.936507'$ $29$ $-3188$ $72$ $-17$ $64.841269841$ $32.936507'$ $29$ $-3188$ $72$ $-17$ $64.841269841$ $32.936507'$ $30$ $-3233$ $72$ $-23$ $56.031746032$ $41.507936'$ $31$ $-1637$ $72$ $-19$ $61.746031746$ $36.063492'$ $32$ $-1682$ $72$ $-26$ $50.00000000$ $47.698412'$ $33$ $-1689$ $72$ $-25$ $52.777777778$ $44.920634'$ $34$ $-1694$ $72$ $-28$ $47.857142857$ $49.603174'$ $35$ $-1711$ $72$ $-20$ $62.444444444$ $51.158730'$ $36$ $-1781$ $72$ $-28$ $50.317460317$ $47.619047'$ $37$ $-1636$ $65$ $-25$ $55.881886014$ $41.974916'$ $38$ $-1736$ $65$ $-14$ $73.015873016$ $24.761904'$ $39$ $-1759$ $65$ $-26$ $55.396825397$ $42.698412'$ $40$ $-1657$ $65$ $-31$ $47.539682540$ $50.158730'$ $41$ $-1591$ $65$ $-28$ $53.09523809524$ $28.015873'$ $42$ $-1934$ $65$ $-17$ $69.761904762$ $28.015873'$ $43$ $-1506$ $70$ $-17$ $69.5238095$	873
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	730
28 $-3138$ $72$ $-15$ $67.857142857$ $29.9365079$ $29$ $-3188$ $72$ $-17$ $64.841269841$ $32.9365079$ $30$ $-3233$ $72$ $-23$ $56.031746032$ $41.5079363$ $31$ $-1637$ $72$ $-19$ $61.746031746$ $36.0634920$ $32$ $-1682$ $72$ $-26$ $50.000000000$ $47.6984129$ $32$ $-1682$ $72$ $-25$ $52.777777778$ $44.9206349$ $34$ $-1694$ $72$ $-28$ $47.857142857$ $49.60317469$ $35$ $-1711$ $72$ $-20$ $62.444444444$ $51.158730$ $36$ $-1781$ $72$ $-28$ $50.317460317$ $47.61904769$ $37$ $-1636$ $65$ $-25$ $55.881886014$ $41.97491669$ $38$ $-1736$ $65$ $-14$ $73.015873016$ $24.761904769$ $39$ $-1759$ $65$ $-26$ $55.396825397$ $42.69841296666941296666666666676666666666666666666666666$	583
29 $-3188$ $72$ $-17$ $64.841269841$ $32.9365079$ $30$ $-3233$ $72$ $-23$ $56.031746032$ $41.5079363$ $31$ $-1637$ $72$ $-19$ $61.746031746$ $36.0634920$ $32$ $-1682$ $72$ $-26$ $50.000000000$ $47.6984120$ $33$ $-1689$ $72$ $-25$ $52.77777778$ $44.9206349$ $34$ $-1694$ $72$ $-28$ $47.857142857$ $49.60317460317460317460317460317460317460317460317460317460317435-171172-2062.444444444451.158730036-178172-2850.31746031747.619047603666656666666666666666666666666666666$	937
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	937
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	598
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35         -1711         72         -20         62.44444444         51.158730           36         -1781         72         -28         50.317460317         47.6190470           37         -1636         65         -25         55.881886014         41.9749160           38         -1736         65         -14         73.015873016         24.76190470           39         -1759         65         -26         55.396825397         42.6984120           40         -1657         65         -31         47.539682540         50.158730           41         -1591         65         -28         53.095238095         44.5238093           42         -1934         65         -17         69.761904762         28.0158730           43         -1506         70         -17         69.523809524         28.0158730	503
36         -1781         72         -28         50.317460317         47.6190476           37         -1636         65         -25         55.881886014         41.9749166           38         -1736         65         -14         73.015873016         24.7619047           39         -1759         65         -26         55.396825397         42.6984126           40         -1657         65         -31         47.539682540         50.158730           41         -1591         65         -28         53.095238095         44.5238095           42         -1934         65         -17         69.761904762         28.0158730           43         -1506         70         -17         69.523809524         28.0158730	159
37         -1636         65         -25         55.881886014         41.9749160           38         -1736         65         -14         73.015873016         24.761904'           39         -1759         65         -26         55.396825397         42.6984120           40         -1657         65         -31         47.539682540         50.158730           41         -1591         65         -28         53.095238095         44.5238093           42         -1934         65         -17         69.761904762         28.0158730           43         -1506         70         -17         69.523809524         28.0158730	519
38         -1736         65         -14         73.015873016         24.761904'           39         -1759         65         -26         55.396825397         42.6984120           40         -1657         65         -31         47.539682540         50.158730           41         -1591         65         -28         53.095238095         44.523809           42         -1934         65         -17         69.761904762         28.0158730           43         -1506         70         -17         69.523809524         28.0158730	553
39         -1759         65         -26         55.396825397         42.6984120           40         -1657         65         -31         47.539682540         50.158730           41         -1591         65         -28         53.095238095         44.5238093           42         -1934         65         -17         69.761904762         28.0158730           43         -1506         70         -17         69.523809524         28.0158730	762
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	598
41         -1591         65         -28         53.095238095         44.5238095           42         -1934         65         -17         69.761904762         28.0158730           43         -1506         70         -17         69.523809524         28.0158730           44         1402         70         -18         69.646750848         20.1206054	159
42         -1934         65         -17         69.761904762         28.0158730           43         -1506         70         -17         69.523809524         28.0158730           44         1402         70         -17         69.646750248         20.1206060	524
43 -1506 70 -17 69.523809524 28.0158730 44 1402 70 19 69.64735049 20.1296730	)16
	016
44 -1493 /0 -18 08.040/09848 29.129606	)99
45 -1669 70 -17 70.55555556 27.253968	254
46 -1520 70 -29 52 539682540 45 444444	<u>-</u>
47 -1520 70 -29 52.253968254 45 555555	556
48 -2501 70 -28 54 920634921 42 9841269	984

49	-2421	70	-28	55.317460317	42.650793651
50	-3149	74	-28	54.809523810	42.857142857
51	-3469	74	-26	58.269841270	39.365079365
52	-4919	74	-26	58.746031746	38.809523810
53	-4925	74	-31	50.650793651	46.873015873
54	-5725	74	-19	70.793650794	26.984126984
55	-5694	74	-27	59.126984127	38.809523810
56	-5111	74	-31	51.507936508	46.190476190
Tal	la Jas F		montol	Critical Value	a Obtained(1)

 Table 2a: Experimental Critical Values Obtained(1)

NN	CV6	CV7	CV8	CV9
7	71.984126984	2.698412698	25.317460317	-195
8	72.015281757	2.690226043	25.294492200	-195
9	74.523809524	2.142857143	23.333333333	-266
10	76.190476190	2.460317460	21.349206349	-239
11	78.253968254	1.746031746	20.000000000	-246
12	79.332273450	2.082670906	18.585055644	-253
13	79.682539683	2.095238095	18.22222222	-286
14	81.349206349	1.857142857	16.793650794	-304
15	82.619047619	1.984126984	15.396825397	-309
16	83.809523810	1.428571429	14.761904762	-279
17	84.841269841	1.269841270	13.888888889	-315
18	85.476190476	1.349206349	13.174603175	-294
19	86.269841270	1.904761905	11.825396825	-299
20	87.142857143	1.111111111	11.746031746	-314
21	87.698412698	1.031746032	11.269841270	-344
22	88.095238095	1.587301587	10.317460317	-358
23	88.095238095	1.746031746	10.158730159	-374
24	88.730158730	1.587301587	9.682539683	-377
25	88.968253968	1.587301587	9.44444444	-384
26	88.968253968	1.031746032	10.00000000	-386
27	89.047619048	1.269841270	9.682539683	-393
28	89.920634921	0.873015873	9.206349206	-415
29	90.238095238	1.031746032	8.730158730	-411
30	90.015873016	0.936507937	9.047619048	-424
31	89.682539683	1.253968254	9.063492063	-418
32	90.634920635	0.714285714	8.650793651	-428
33	90.365079365	0.904761905	8.730158730	-424
34	90.317460317	0.873015873	8.809523810	-435
35	90.396825397	0.476190476	9.126984127	-427
36	90.396825397	0.714285714	8.888888889	-437
37	90.950944594	0.555643753	8.493411653	-439
38	91.428571429	0.555555556	8.015873016	-437
39	91.349206349	0.952380952	7.698412698	-436
40	92.063492063	0.634920635	7.301587302	-431
41	91.428571429	0.634920635	7.936507937	-458
42	91.666666667	0.634920635	7.698412698	-441
43	91.984126984	0.714285714	7.301587302	-406
44	92.137865311	0.635324015	7.226810673	-439
45	91.666666667	0.634920635	7.698412698	-428
46	91.825396825	0.793650794	7.380952381	-403
47	91.984126984	0.634920635	7.380952381	-411
48	92.380952381	0.793650794	6.825396825	-422
49	92.619047619	0.476190476	6.904761905	-424
50	92.777777778	0.873015873	6.349206349	-409
51	92.77777778	0.952380952	6.269841270	-435
52	92.857142857	0.634920635	6.507936508	-446
53	92.698412698	0.873015873	6.428571429	-480
54	92.936507937	1.031746032	6.031746032	-438



Table 2b: Experimental Critical Values Obtained(2)				
56	93.095238095	0.793650794	6.111111111	-444
55	93.015873016	0.873015873	6.111111111	-437

# 3. Critical Values Trend Analyses- Metric OLNTNES.

# 3.0 General Procedure Adopted.

The tabulated data for each OLNTNES CV is plotted on gnuplot over Linux. Graphical analysis using smooth bezier support and "Fit" command is performed. General observations, for each such graph obtained is reported. Again, various equations of fit are attempted and their summary report is presented for each OLNTNES critical value. Ultimately, choice is made considering firstly value of least reduced chisquare and secondly on most plausible extendability produced at node numbers 80, 100 and 120. Finally, the values of parameters for each equation of each OLNTNES critical value is also noted.

# <u> 3.1 Trend Analysis – OLNTNES CV1.</u>

The curve obtained appears to be oscillating along a mildly decreasing straight line.



Figure 1: OLNTNES Critical Value 1

The applicable equation is:

F(x) = a \* sin (b\*(x-c)) + (d\*x) + fCh\_sq = 435 165 F(80) = -6928.628 224 615F(100)=-9045.150 284 556 F(120)=-12903.691 101 643

The parameters for best fit are:  $a = -2 \ 008.26$ ,  $b = -0.131 \ 905$ ,  $c = 30.317 \ 5$ , d = -102.241, f = 714.647

### 3.2 Trend Analysis – OLNTNES CV2.

The curve obtained appears to be oscillating along a mildly increasing straight line.

The applicable equation is:

F(x)	= ;	a *	sin	(b*	(x-c))	+	(d*x)	+	f
Ch_s	sq = 8	8.556	6		F(80) =	131	.103 575	167	
F(10	0) =	161.3	56 675	540	F(120) =	= 15	9.897 731	32	8

The parameters for best fit are:  $a = -17.751 \ 8$ ,  $b = 0.080 \ 438 \ 2$ ,  $c = 34.771 \ 6$ ,  $d=1.171 \ 65$ ,  $f= 28.915 \ 4$ 



# <u> 3.3 Trend Analysis – OLNTNES CV3.</u>

The curve appears to be an oscillation along an axis which is itself mostly decreasing at a decreasing rate.



The applicable equation is:

$F(x) = a \exp((b * x) + c)$	+d+ f*sin (g*(x-h))
Ch_sq = 23.576 2	F(80) = -23.652 835 588
F(100) = -26.051 612 639	F(120) = -28.844 576 575

The parameters for best fit are:

 $a\,=\,0.466\,\,63$  ,  $b\,=\,-0.056\,\,687\,\,1$  ,  $c\,=\,4.413\,\,03$  ,  $d{=}{-}\,27.333\,8$  ,  $f{=}\,3.797\,\,18$  ,  $g{=}\,0.350\,\,609$  ,  $h{=}\,38.154\,\,2$ 

## <u> 3.4 Trend Analysis – OLNTNES CV4.</u>

The curve appears to be a damped oscillation along a straight line axis.

The applicable equation is:

F(x) =a\*exp(-b\*(x-c))\*cos (2\*b\*pi\*(x-c))+d Ch\_sq = 60.045 2 F(80) = 60.611 214 791 F(100) = 60.409 652 824 F(120) = 60.396 045 522

The parameters for best fit are:  $a=0.326\ 901$  ,  $b=0.056\ 740\ 9$  ,  $c=77.643\ 8$  ,  $d{=}60.420\ 3$ 





### 3.5 Trend Analysis - OLNTNES CV5.

The curve appears to be a case of damped oscillation along a straight line of positive gradient.



The applicable equation is:

 $F(x) = a^{exp(-b^{(x-c)}) cos} (2^{b^{ey}(x-c)}) + d^{ex+f}$   $Ch_sq = 58.232 \quad F(80) = 44.208$   $F(100) = 47.587 \quad F(120) = 50.784$ 

The parameters for best fit are:  $a = 0.555\ 039$ ,  $b = 0.055\ 223\ 4$ ,  $c = 69.935\ 6$ ,  $d = 0.156\ 838$ ,  $f = 31.960\ 5$ 

## <u>3.6 Trend Analysis – OLNTNES CV6.</u>

Generally, the curve obtained here increases at a decreasing rate.



The potentially applicable equations are:

1. $F(x) = a * exp (b * x) + (c*x) + d$
$Ch_{sq} = 2.022\ 36 \qquad F(80) = 73.229\ 969\ 576$
F(100)=41.240 240 974 F(120)= -9.402 767 677
2. $F(x) = a * log (b * x) + (c*x) + d$
$Ch_{sq} = 0.337\ 59 \qquad F(80) = 90.215\ 653\ 731$
F(100)=87.021 027 428 F(120)=83.050 373 205
3. $F(x) = a * x * log (b*x) + (c*x) + d$
$Ch_{sq} = 1.479\ 37 \qquad F(80) = 79.133\ 546\ 229$
F(100)=60.833 938 529 F(120)=35.779 809 566
4. $F(x) = a * x^{-1} * \log (b*x) + (c*x) + d$
$Ch_{sq} = 0.276\ 054 \qquad F(80) = 91.772\ 595\ 111$
F(100)= 90.024 681 483 F(120)=87.669 003 515
5. $F(x) = a * x^{-2} * \log (b*x) + (c*x) + d$
$Ch_{sq} = 0.154\ 076 \qquad F(80) = 93.525\ 391\ 724$
F(100)= 93.783 756 188 F(120)=93.918 874 884
6. $F(x) = a * x^{-2.5} * log (b*x) + (c*x) + d$
$Ch_{sq} = 0.125 \ 2 \qquad F(80) = 94.763 \ 990 \ 385$
$F(100) = 96.198\ 222\ 062$ $F(120) = 97.708\ 848\ 375$

## **Choice of best fit for SLNTNES Critical Value 6**

The equation in part 6 above has been selected because of smallest reduced chi-square value obtained and good extendability. The parameters obtained for best fit are:

a = -6 979.98, b= 0.207 054, c= 0.004 582 22, d= 91.827 5

# <u>3.7 Trend Analysis – OLNTNES CV7.</u>

Generally, the curve depicts a decreasing tendency until a minimum point, then shows an increasing tendency. The curve obtained depicts about half a wave:



The applicable equation is:

F(x) = a \* sin ((b\* x) + c) + dCh\_sq = 0.051 681 1 F(80) = 2.511 931 649

 $F(100) = 4.714\ 178\ 503$   $F(120) = 7.217\ 407\ 852$ 

# The parameters obtained for best fit are:

a= 5.462 12, b= 0.023 133 4, c= -3.704 69, d= 6.145 59



# <u>3.8 Trend Analysis – OLNTNES CV8.</u>

Generally, the curve depicts a decreasing tendency at a decreasing rate.



The potentially applicable equations are:

1.F(x) = a * exp ((b)	* x ) +c) + d
$Ch_{sq} = 0.313578$	$F(80) = 6.714\ 650\ 734$
F(100)=6.702 133 122	F(120)=6.700 395 627
2.F(x) = a * x * exp	((b*x) +c) + d
Ch_sq = 0.458 186	F(80) = 7.297 253 417
F(100)= 7.297 017 203	F(120)=7.297 010 154
3. $F(x) = a * x^{0.25} * e$	xp ((b*x)+c) + d
$Ch_{sq} = 0.330\ 081$	F(80) = 6.906 314 392
F(100)=6.901 578 184	F(120) = 6.901 129 765
4.F(x) = a * exp ((b))	*x)+c) + (d * x)
$Ch_{sq} = 0.553\ 51$	F(80)= 9.312 487 067
F(100)=11.474 049 413	F(120)=13.728 599 970

### **Choice of best fit for SLNTNES Critical Value 8**

The equation in part 1 above has been selected because of smallest reduced chi-square value obtained and good extendability. The parameters obtained for best fit are:

a = 4.207 32, b= -0.098 734 6, c= 2.230 76, d= 6.700 12

# <u>3.9 Trend Analysis – OLNTNES CV9.</u>

The curve obtained here shows decreasing tendency at a decreasing rate.



Figure 9: OLNTNES Critical Value 9

The potentially applicable equations are:

1. $F(x) = a / log ((b * x) + c) + d$
$Ch_{sq} = 457.98$ $F(80) = -476.583\ 896\ 683$
F(100)=-487.959 017 824 F(120)=-495.801 903 894
2. $F(x) = a * exp ((b * x) + c) + d$
$Ch_{sq} = 392.467 \qquad F(80) = -453.443\ 377\ 428$
F(100)=-454.705 519 396 F(120)=-455.020 239 560
3. $F(x) = a * exp ((b*x)+c) + (d*x^{0.25})$
$Ch_{sq} = 388.584$ $F(80) = -391.151\ 211\ 570$
F(100)=-308.479 987 522 F(120)=-188.195 841 981
4. $F(x) = a * exp ((b*x)+c) + (d*x^{0.5})$
Ch_sq = $366.868$ F(80) = $-216.488730936$
F(100)=252.313 505 313 F(120)= 1 210.880 853 749

# **Choice of best fit for SLNTNES Critical Value 9**

The equation in part 2 above has been selected because of smallest reduced chi-square value obtained and good extendability. The parameters obtained for best fit are:

a = 14.178 1, b= -0.069 444 1, c= 3.423 46, d= -455.125

# 4. Conclusion.

This piece of research was aimed at and has as achievement the identification of some critical values relevant to metric OLNTNES and modelling of their corresponding trends over varying node densities in a MANET topography of  $300 \times 300 \text{ m}^2$ . The models put forward comprise of mathematical equations of varying complexity levels which will assist in studying MANETs for MAUC environment from a software engineering perspective. These mathematical models may fairly easily be implemented as programming algorithms, to generate more rigorously realistic simulation scenarios with the help of which newly developed communication protocols and middleware components for ubicomp may be tested.

This experiment has been conducted in NS-2 over Linux. The plottings and "Fit" attempts were carried out in gnuplot. Best fit was selected based on least reduced chi-square values and best extendability of equations at higher node numbers have been used. Assumptions stated in previous papers [17, 33] are continued here also.

This work is a follow-up of previous papers [1-13, 17, 33] and remains open for future upgrades. One such further work identified is formulating a method of predictability for metric OLNTNES and its trend.

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